VOLTAGE DELAY AND COMPLEX IMPEDANCE CHARACTERISTICS OF A HIGH-RATE LITHIUM/SILVER-VANADIUM OXIDE MULTIPLATE BATTERY (EXTENDED ABSTRACT)

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A high-rate, multiplate lithium/organic electrolyte/silver-vanadium oxide system has been developed to power implantable cardiac defibrillators [1]. Room temperature voltage delay and complex impedance analyses have been completed on five rectangular cells (dimensions: 13.5 mm \times 52 mm \times 21 mm; external volume: 14.6 cm³; theoretical capacity: 3.0 A h) at different depths of discharge.

After manufacture, 2% of each cell's theoretical capacity was extracted and the cells were allowed to rest for one month. A 2.0 A, 10 s pulse was then applied to record voltage delay. Figure 1 presents an example of the recorded voltage response. Initial open circuit voltages ranged from 3240 to 3260 mV; initial 2.0 A voltages ranged from 2355 to 2410 mV; initial 2.0 A voltage drops ranged from 850 to 905 mV; final 2.0 A voltages ranged from 2500 to 2550 mV.



Fig. 1. Voltage delay during a 10 s 2.0 A pulse.

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Fig. 2. Equivalent circuit model for complex impedance response:

 $Z_{\mathbf{R}_1} = R_1$ $Z_{L} = J_{\omega L}$ $Z_{2} = ((R_{2})^{-1} + (J\omega)^{\eta_{2}}C_{2})^{-1}$ $Z_{3} = ((R_{3} + Z_{w})^{-1} + (J\omega)^{\eta_{3}}C_{3})^{-1}$ where $J = \sqrt{-1}$ = Angular frequency $\omega = 2\pi F$ $R_1, R_2, R_3 = \text{Resistive components } (\Omega)$ = Inductive component (H) L C_1, C_2, C_3 = Capacitive components (F) Z_{w} K = Warburg impedance contribution = $K(1-J)/\sqrt{\omega}$ = Warburg coefficient $= 1 - \theta_{2,3}/90.0$ η_2, η_3 = Angles of deviation from ideal symmetry about the -Imag Z = 0 axis θ_2, θ_3 (degrees).



Fig. 3. Complex impedance results before pulse discharge (av. of 4 cells). $R_1 = 0.09 \Omega$, $R_2 = 0.94 \Omega$, $R_3 = 0.09 \Omega$; K = 0.099, $L = 0.0212 \mu$ H, $C_2 = 0.0013$ F, $C_3 = 0.7814$ F.

During the one month storage period, complex impedance responses were obtained on four cells over the frequency range $0.01 \cdot 100\,000$ Hertz using a PAR Model 368 a.c. impedance measurement system. Results were then integrated with an equivalent circuit model (Fig. 2) developed from the work of Mauger *et al.* [2], and circuit parameters were obtained using the relationships shown below.

Figure 3 presents the Nyquist and Bode graphs for the average of the modeled complex impedance responses along with the resulting circuit parameters.

The test cells then went through a regime of partial discharge (using 2.0 A, 10 s pulses with four pulses per train, 15 s of rest between pulses, and 30 min of rest between pulse trains), storage, complex impedance and voltage delay testing until they reached end-of-life (1.7 V under the 2.0 A pulse load). Voltage delay and complex impedance analyses were completed at each depth of discharge, and trends in the initial 2.0 A voltages and the complex impedance equivalent circuit parameters were noted as functions of depth of discharge.

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